

Calibration II

Dharam V. Lal

**with due thanks to several friends / collaborators at
UCT, IDIA (SA), NCRA-TIFR (India) and NRAO (USA)**

TELESCOPE SENSITIVITY

Noise limit for imaging with interferometric radio telescopes

$$\sigma = \frac{T_{\text{sys}}}{A_{\text{eff}} \times \sqrt{(\Delta\nu \times \Delta t)}}$$

Sensitivity improvements achieved by

- wide band receivers,
- long integration times
- more antennas
- long baselines

$$\sigma_{\text{confusion}} \propto (\nu^{-2.7} / B_{\text{max}}^2)$$

■ $B_{\text{max}} \sim 100 \text{ km @ } 200 \text{ MHz}$, the confusion noise is $\sim 1 \mu\text{Jy beam}^{-1}$.

IMAGING CHALLENGES AT LOW FREQ.

- Wide-field imaging
 - account for direction dependent (DD) effects
 - PB: time, frequency and polarisation dependence
 - w -term
- Wide-band imaging
 - ... plus frequency dependence of the sky brightness
- Data volume $\propto N_{\text{ant}}^2 \times N_{\text{channel}} \times t$
- Sky brightness \implies multi-scale deconvolution
- Ionospheric effects \implies need for DD solvers

IMPLICATIONS FOR IMAGING

Long baselines $B_{\max} > 2 \text{ km} \implies \text{DR} > 10^4$

Wide-field effects:

- w -term, PB effects and ionosphere effects

Larger data volume

Wide-field, wide-band, high resolution, high dynamic range imaging using large data sizes

- a natural consequence of low frequency and high sensitivity imaging.

CALIBRATION AND IMAGING

- Standard calibration and imaging

- (DI instrumental effects)

- w/ DD instrumental + propagation effects

- correction for w -term and for PB

- image plane correction
 - Fourier plane correction
 - pointing self-calibration

- Mosaicing

- w/ advanced image parameterisation

- multi-scale CLEAN (deconvolution)
 - multi-frequency synthesis (imaging)
 - full polarisation (Stokes) calibration and imaging

MEASUREMENT EQUATION

$$\vec{V}_{ij}^{Obs}(\nu, t) = G_{ij} W_{ij}(\nu, t) \int P_{ij} M_{ij}(s, \nu, t) \vec{I}(s, \nu) e^{i\vec{b}_{ij} \cdot \vec{s}} d\vec{s}$$

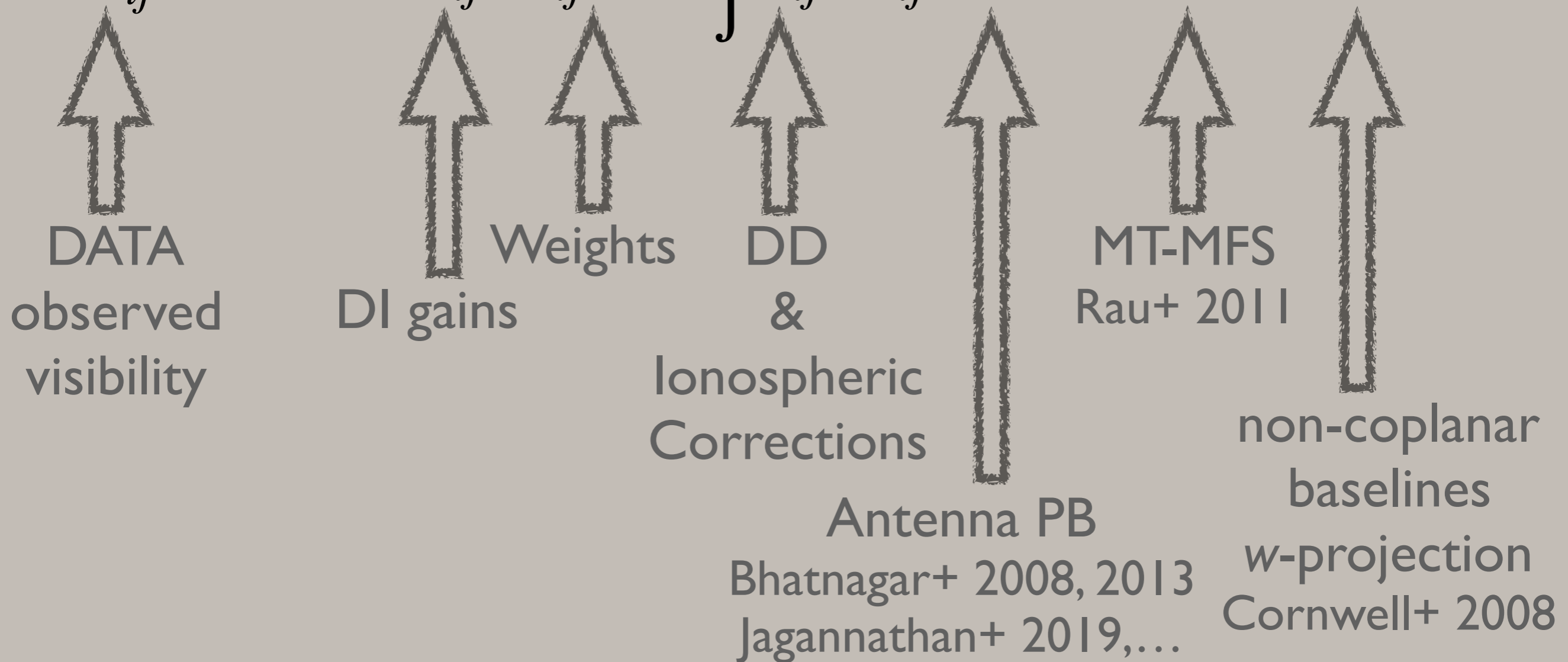
MEASUREMENT EQUATION

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$$V(u, v, w) = \int \frac{I(l, m, n)}{n} e^{-2\pi i(ul + vm + w(n-1))} dl dm$$

MEASUREMENT EQUATION

$$\vec{V}_{ij}^{Obs}(\nu, t) = G_{ij} W_{ij}(\nu, t) \int P_{ij} M_{ij}(s, \nu, t) \vec{I}(s, \nu) e^{i\vec{b}_{ij} \cdot \vec{s}} d\vec{s}$$



MEASUREMENT EQUATION

$$\Gamma(\vec{b}) = \int \left\langle E(\vec{s}, t) \cdot E^*(\vec{s}, t - \vec{b} \cdot \vec{s}/c) \right\rangle e^{-2\pi i \vec{b} \cdot \vec{s}/\lambda} d\Omega$$

mutual
coherence
function

complex amplitude
of the radiation
emanating from the
source in the
direction \vec{s}

$\vec{s} = \vec{s}_0 + \vec{\sigma}$
point near
the phase
centre

time difference
between the
incoming radiation
collected at two
antennas separated
by \vec{b}

$$d\Omega = \frac{d\vec{s}}{R^2}$$

MEASUREMENT EQUATION

$$\Gamma(\vec{b}) = \int \left\langle E(\vec{s}, t) \cdot E^*(\vec{s}, t - \vec{b} \cdot \vec{s}/c) \right\rangle e^{-2\pi i \vec{b} \cdot \vec{s}/\lambda} d\Omega$$

$$V(u, v, w) = \int \frac{I(l, m, n)}{n} e^{-2\pi i (ul + vm + w(n-1))} dl dm$$

(for $w \simeq 0, n \simeq 1$)

$$V(u, v) = \int I(l, m) e^{-2\pi i (ul + vm)} dl dm$$

(this is van-Cittert Zernike theorem)

MEASUREMENT EQUATION

$$\Gamma(\vec{b}) = \int \left\langle E(\vec{s}, t) \cdot E^*(\vec{s}, t - \vec{b} \cdot \vec{s}/c) \right\rangle e^{-2\pi i \vec{b} \cdot \vec{s}/\lambda} d\Omega$$

$$V(u, v, w) = \int \frac{I(l, m, n)}{n} e^{-2\pi i (ul + vm + w(n-1))} dl dm$$

Polarised radiation:

$$\vec{E}_i = [E^r \ E^l]_i^T$$

- (two nominal orthogonal components of incident electric field are measured at each antenna i)

MEASUREMENT EQUATION

$$\Gamma(\vec{b}) = \int \left\langle E(\vec{s}, t) \cdot E^*(\vec{s}, t - \vec{b} \cdot \vec{s}/c) \right\rangle e^{-2\pi i \vec{b} \cdot \vec{s}/\lambda} d\Omega$$

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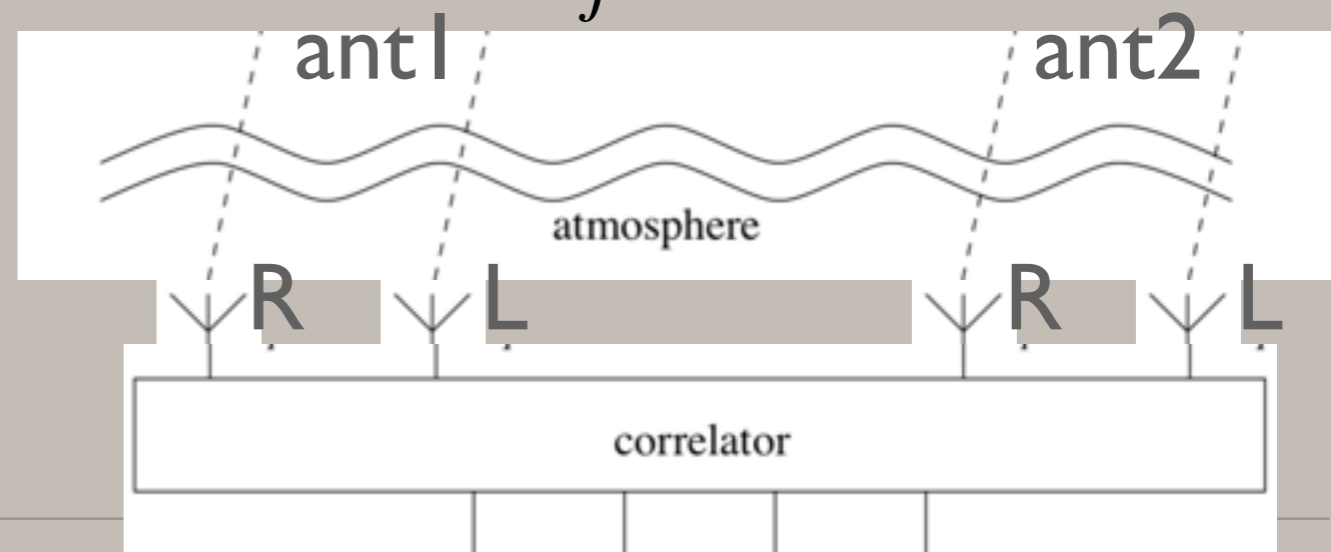
Polarised radiation:

$$\vec{E}_i = [E^r \ E^l]^T_i$$

(four cross-correlation products, $\langle \vec{E}_i \otimes \vec{E}_j^* \rangle$ per baseline)

$$\vec{V}_{ij} = [V^{rr} \ V^{rl} \ V^{lr} \ V^{ll}]^T_{ij}$$

$$\vec{I} = [I^{rr} \ I^{rl} \ I^{lr} \ I^{ll}]^T$$



MEASUREMENT EQUATION

$$\vec{E}_i = [E^r \ E^l]_i^T$$

- (suffers from propagate effects and receiver electronics)

(Jones matrices describe this modulation for the electric field incident at each orthogonal pair of feeds $\vec{E}_i = [E^r \ E^l]_i^T$)

- DI: $J_i^{vis} = [GDC]$

- (a 2×2 matrix product)

- complex gains, G ,
- polar'n leakage, D and
- feed config'n, C .

- DD: $J_i^{sky} = [EPF]$

- (a 2×2 matrix product)

- AIPs, E ,
- PA effects, P and
- tropospheric / ionospheric effects, and Faraday R'n, F .

MEASUREMENT EQUATION

$$\vec{E}_i = [E^r \ E^l]_i^T$$

- (suffers from propagate effects and receiver electronics)

(Jones matrices describe this modulation for the electric field incident at each orthogonal pair of feeds $\vec{E}_i = [E^r \ E^l]_i^T$)

- DI: $J_i^{vis} = [GDC]$

- DD: $J_i^{sky} = [EPF]$

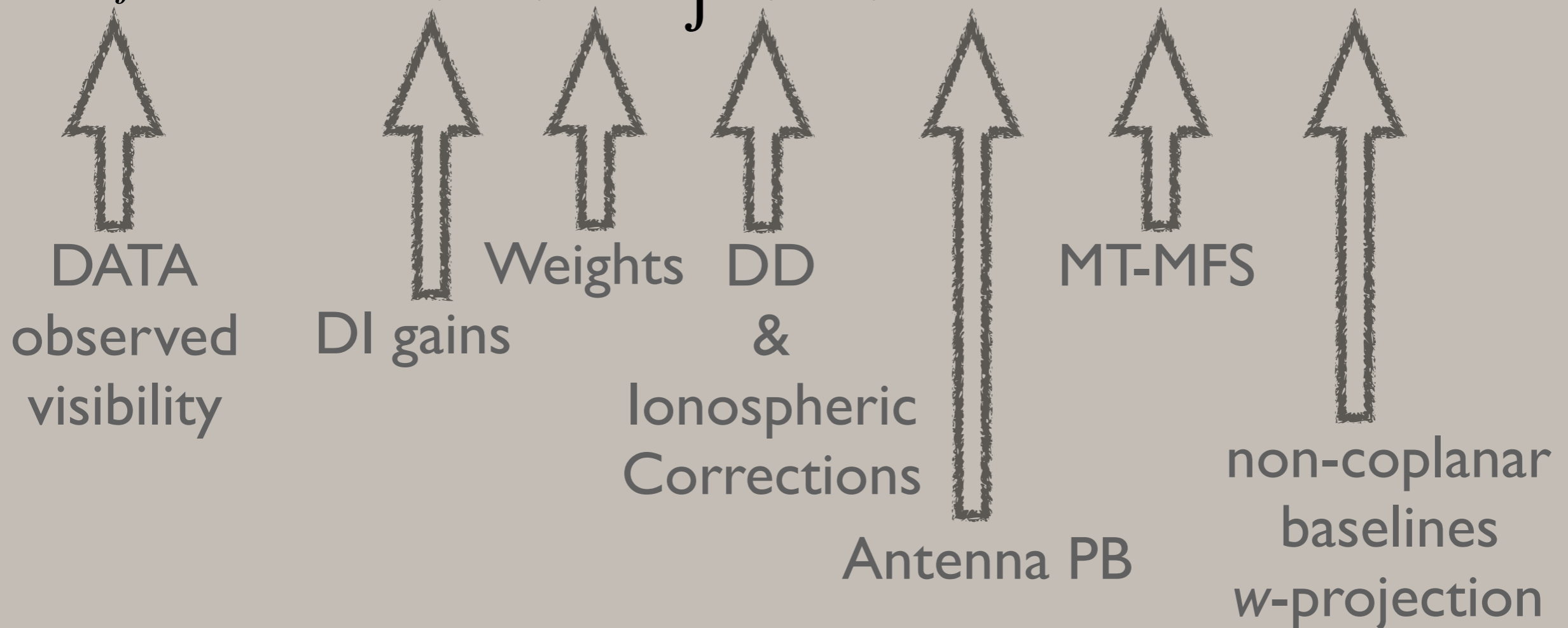
- $K_{ij}^{\{vis, sky\}} = [J_i \otimes J_j^\dagger]^{\{vis, sky\}}$

- (effect on each baseline ij is described by the outer-product of these antenna-based Jones matrices, a 4×4 matrix!)

$$\vec{V}_{ij}^{obs} = [K_{ij}^{vis}] \int [K_{ij}^{sky}] \vec{I}^{sky}(\vec{s}) e^{-2\pi i \vec{b} \cdot \vec{\sigma} / \lambda} d\Omega$$

MEASUREMENT EQUATION

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$$\vec{V}_{ij}^{obs} = [K_{ij}^{vis}] \int [K_{ij}^{sky}] \vec{I}^{sky}(\vec{s}) e^{-2\pi i \vec{b} \cdot \vec{\sigma} / \lambda} d\Omega$$

CALIBRATION AND IMAGING

- Standard calibration and imaging

- (DI instrumental effects)

- w/ DD instrumental + propagation effects

- correction for **w-term** and for **PB**

- image plane** correction

- Fourier plane** correction

- pointing self-calibration

- Mosaicing

- w/ advanced image parameterisation

- multi-scale CLEAN** (deconvolution)

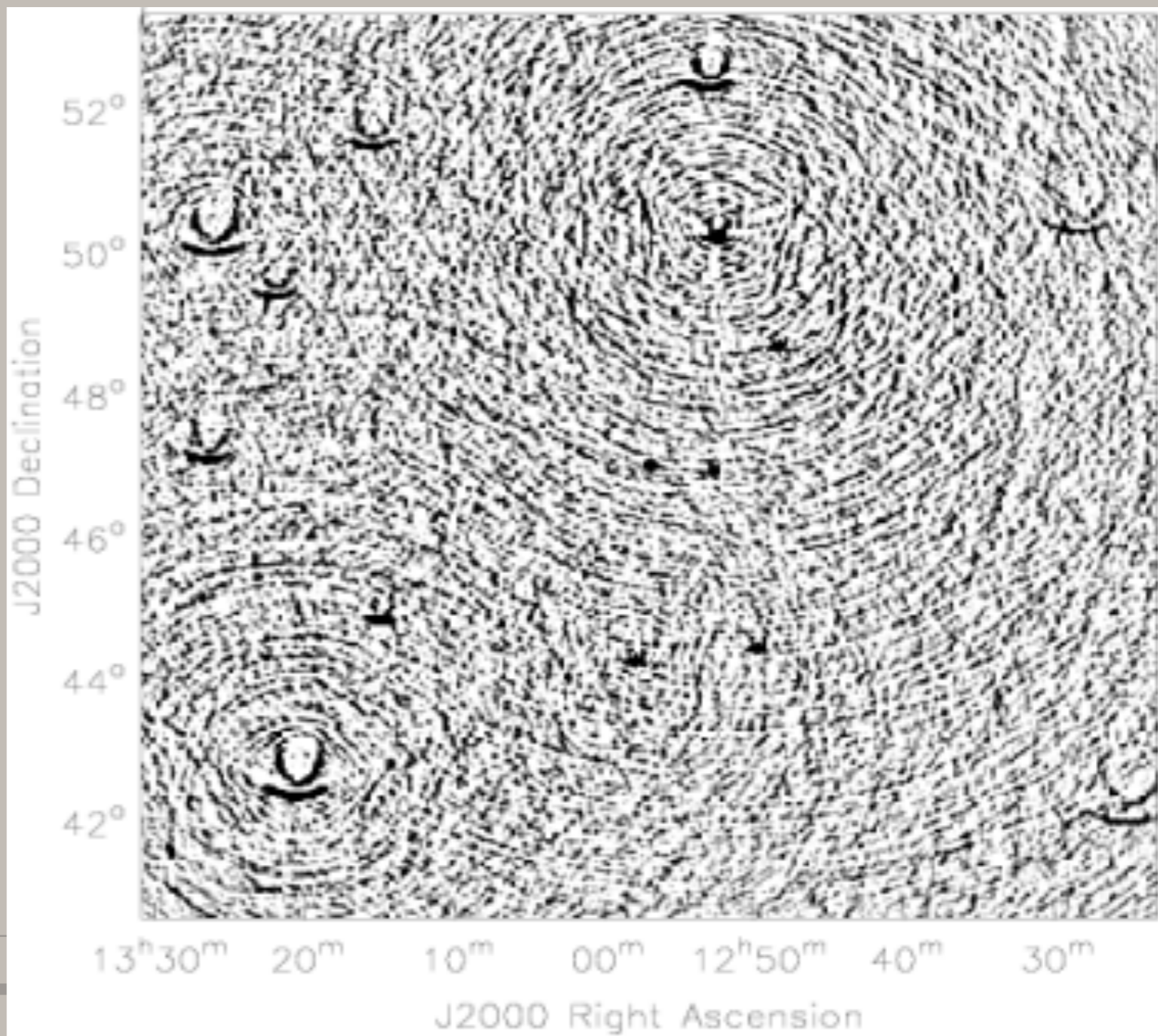
- multi-frequency synthesis** (imaging)

- full polarisation** (Stokes) calibration and imaging

W-TERM

$$V(u, v, w) = \int \frac{I(l, m, n)}{n} e^{-2\pi i(ul+vm+w(n-1))} dl dm$$

$$e^{i w \sqrt{1-l^2-m^2}}$$



Credits: S. Bhatnagar, synthesis
imaging NRAO workshop

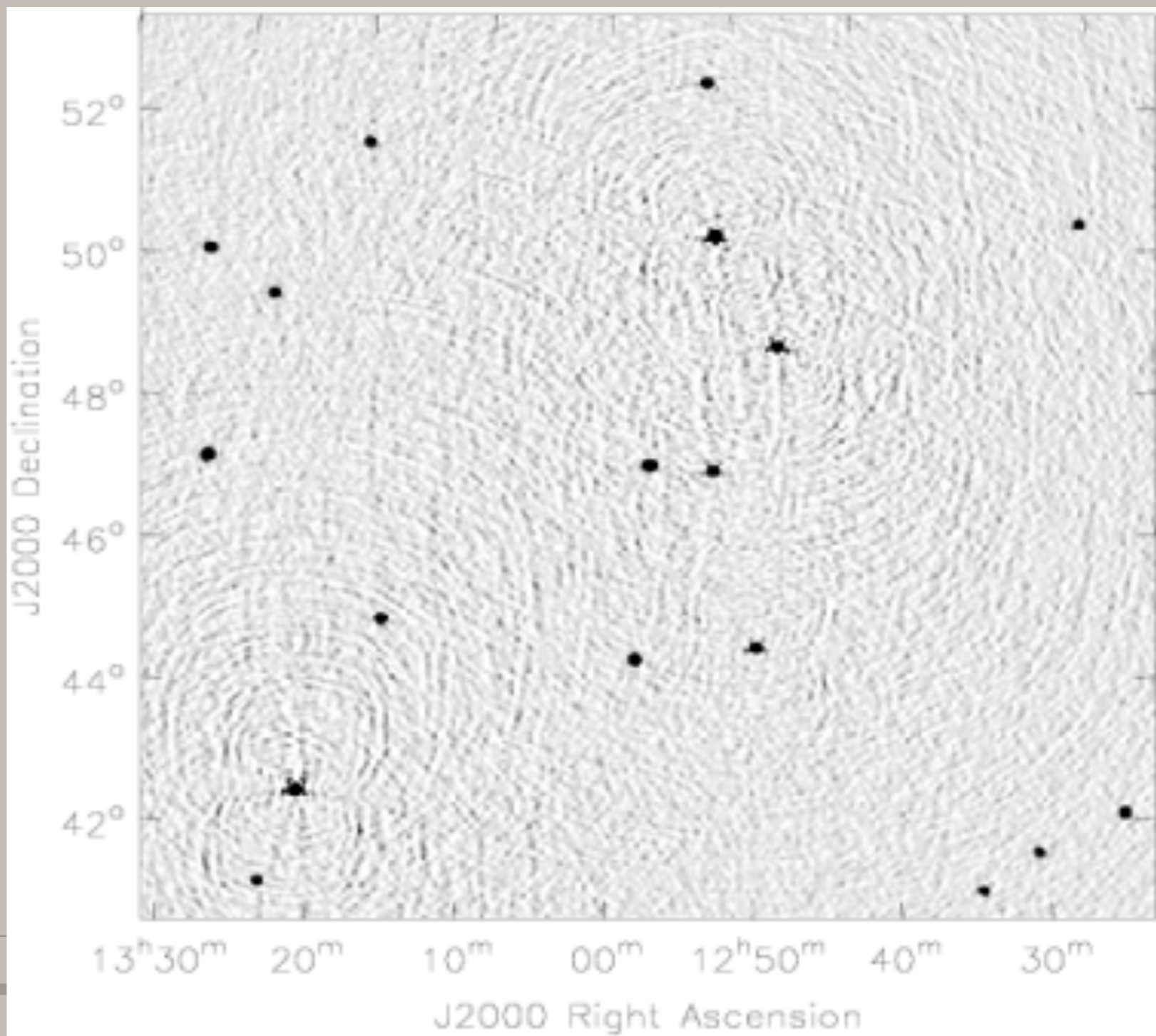
Dharam V. LAL (NCRA-TIFR)

W-TERM

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$$e^{iw\sqrt{1-l^2-m^2}}$$

divide the FoV into
a no. of FACETS



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Dharam V. LAL (NCRA-TIFR)

W-TERM

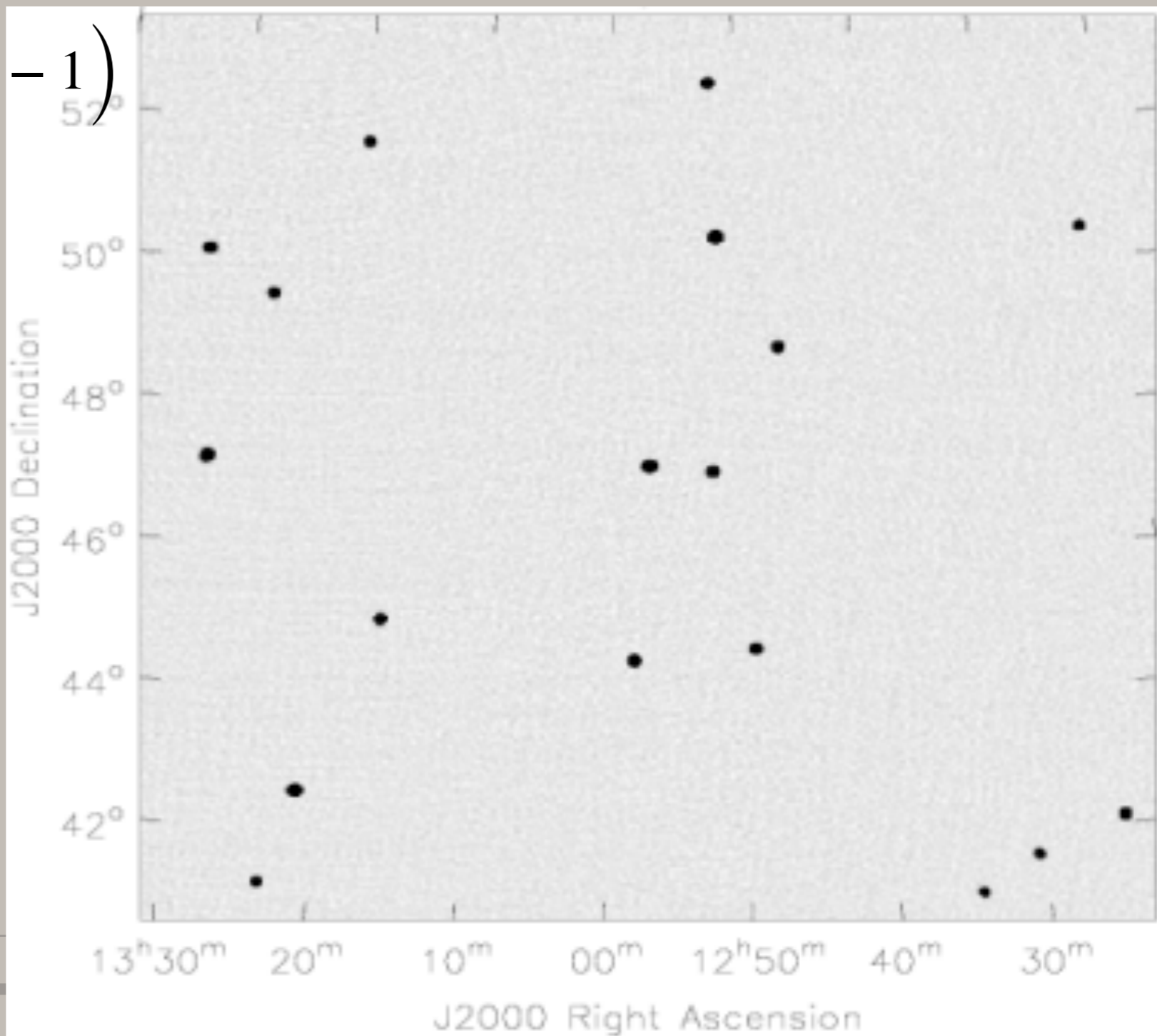
$$V(u, v, w) = \int \frac{I(l, m, n)}{n} e^{-2\pi i(ul+vm+w(n-1))} dl dm$$

$$K_{ij}^{Sky} = e^{w_{ij}(\sqrt{1-l^2-m^2}-1)}$$

An order-of-magnitude faster than FACETing, and for the same amount of computing time provides higher DR images.

Credits: S. Bhatnagar, synthesis imaging NRAO workshop

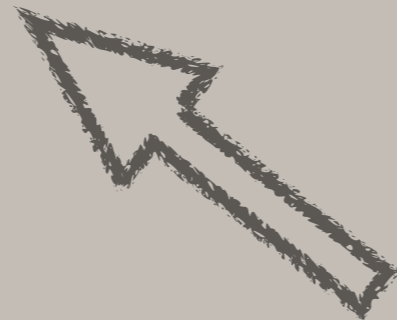
Dharam V. LAL (NCRA-TIFR)



CORRECTION FOR **PB**

A-projection

$$\vec{V}_{ij}^{obs} = [K_{ij}^{vis}] \int [K_{ij}^{sky}] \vec{I}^{sky}(\vec{s}) e^{-2\pi i \vec{b} \cdot \vec{\sigma} / \lambda} d\Omega$$



is different for each baseline

Assumption:

- sky is (not) variable, and
- Antenna power pattern is (not) changing!

CORRECTION FOR **PB****A**-projection

$$\vec{V}_{ij}^{obs} = [K_{ij}^{vis}] \int [K_{ij}^{sky}] \vec{I}^{sky}(\vec{s}) e^{-2\pi i \vec{b} \cdot \vec{\sigma} / \lambda} d\Omega$$

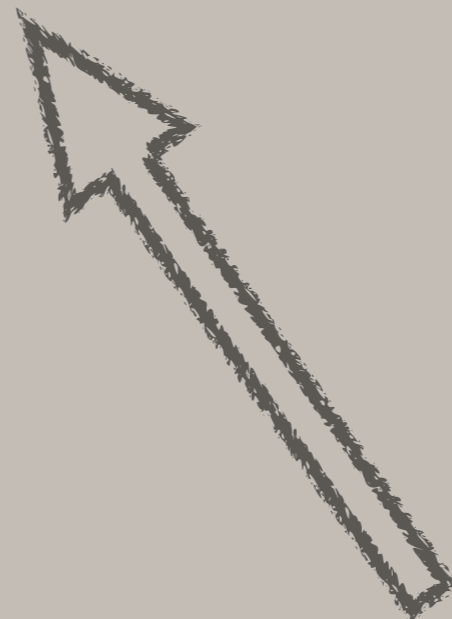
$$\vec{V}_{cn \times 1}^{obs} = [K_{cn \times cn}^{vis}] [S_{cn \times cm}] [F_{cm \times cm}] [K_{cm \times cm}^{sky}] \vec{I}_{cm \times 1}^{sky}$$



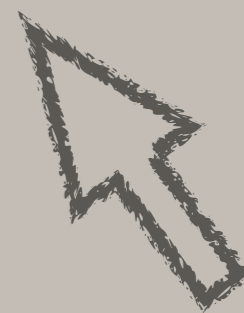
vector of n
visibilities



projection
operator
describing the
uv-coverage



Fourier
transfer
operator



Pixelated
image of sky

CORRECTION FOR **PB**

A-projection

$$\vec{V}_{ij}^{obs} = [K_{ij}^{vis}] \int [K_{ij}^{sky}] \vec{I}^{sky}(\vec{s}) e^{-2\pi i \vec{b} \cdot \vec{\sigma} / \lambda} d\Omega$$

$$\vec{V}_{ij}^{obs}(\nu) = \int J_{ij}^S(s, \nu, t) I(s, \nu) e^{i(ul+vm+w(\sqrt{(1-l^2-m^2)}-1))} ds$$



DATA



PB



SKY



GEOMETRY

- Visibility depends on time and frequency!

CALIBRATION AND IMAGING

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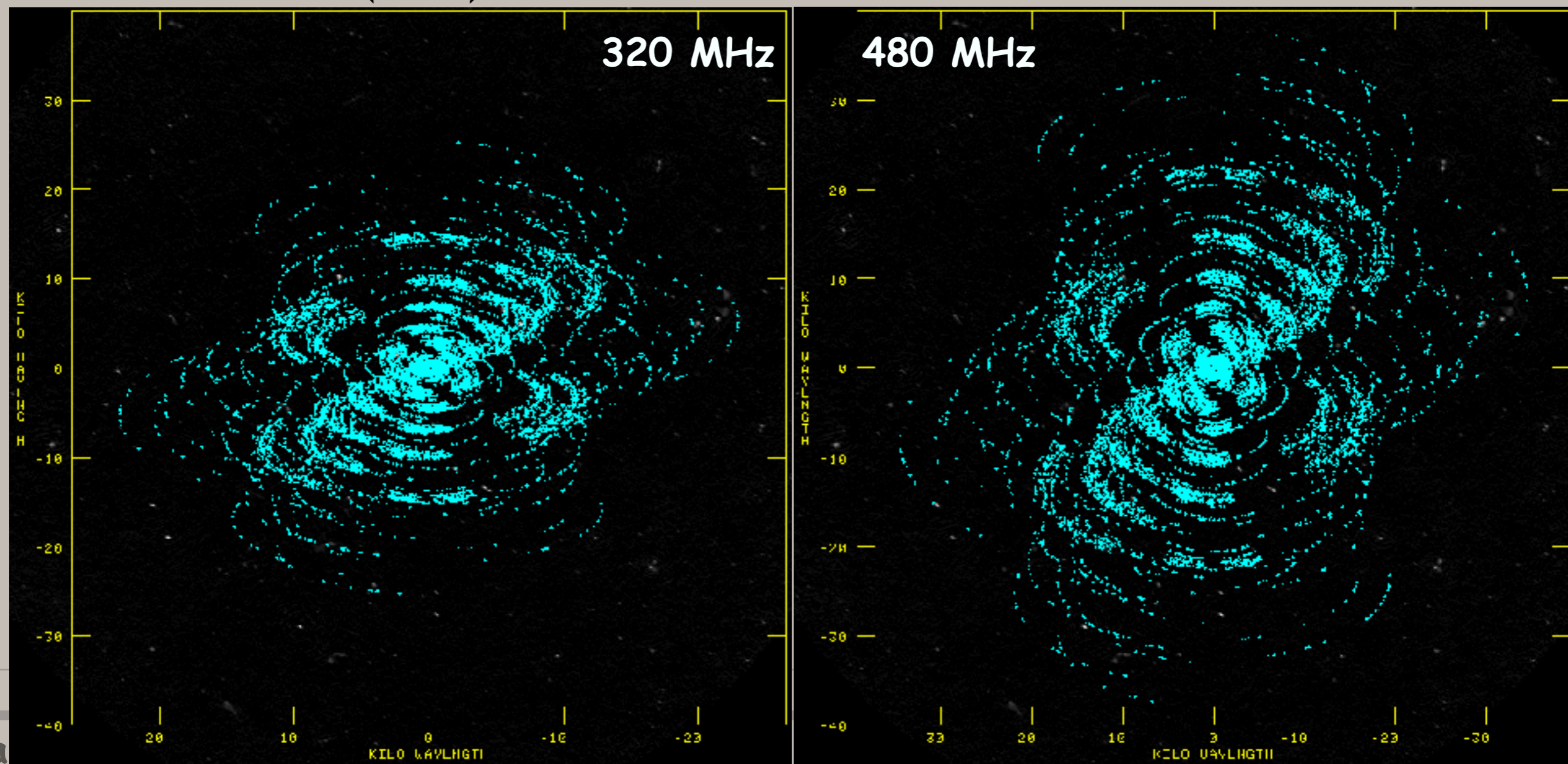
- Mosaicing

- w/ advanced image parameterisation

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 - multi-frequency synthesis** (imaging)
 - full polarisation** (Stokes) calibration and imaging

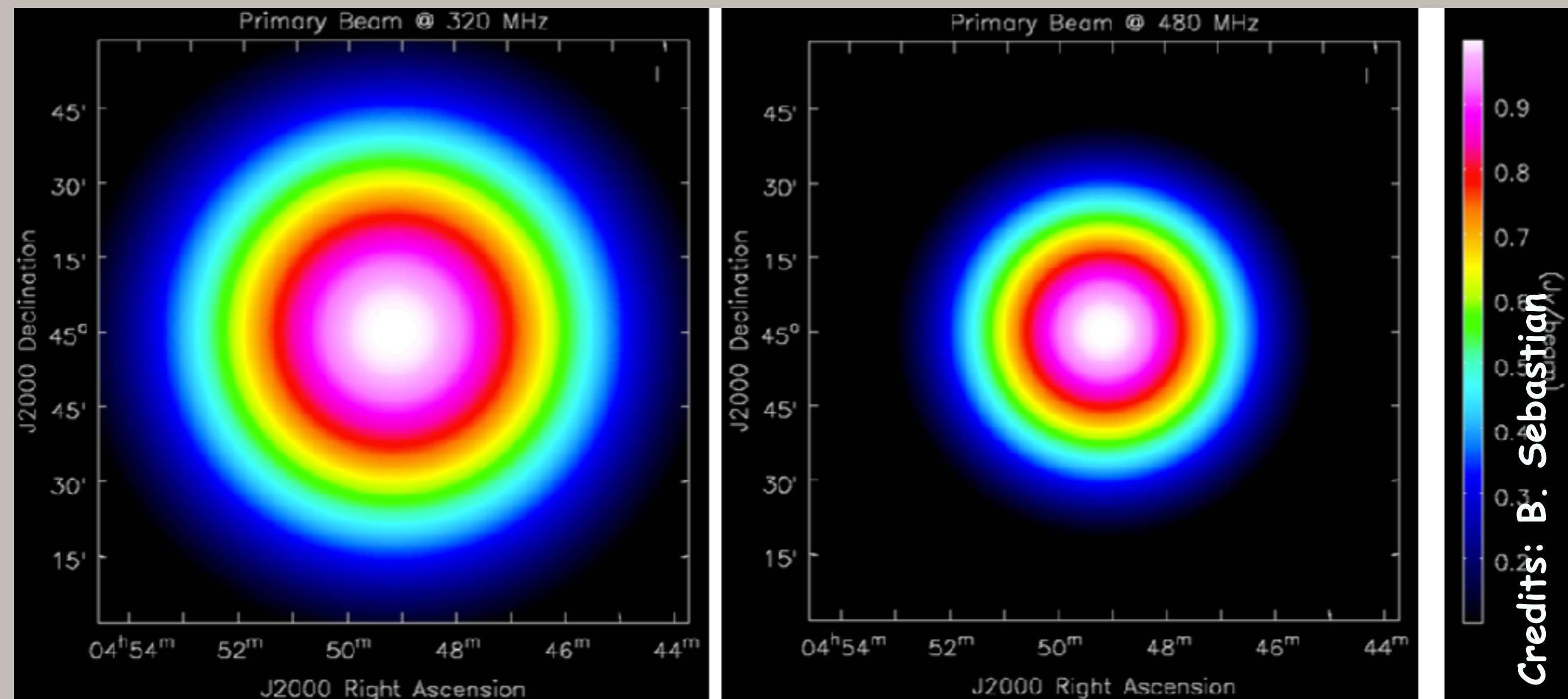
CORRECTION FOR **PB****multi-frequency synthesis**

$$I_{\nu}^{sky} = I_{\nu_0}^{sky} \left(\frac{\nu}{\nu_0} \right)^{I_{\alpha}^{sky} + I_{\beta}^{sky} \log(\frac{\nu}{\nu_0})}$$



CORRECTION FOR **PB****A**-projection

$$\vec{V}_{ij}^{obs}(\nu) = \int J_{ij}^S(s, \nu, t) I(s, \nu) e^{i(ul+vm+w(\sqrt{(1-l^2-m^2)}-1))} ds$$



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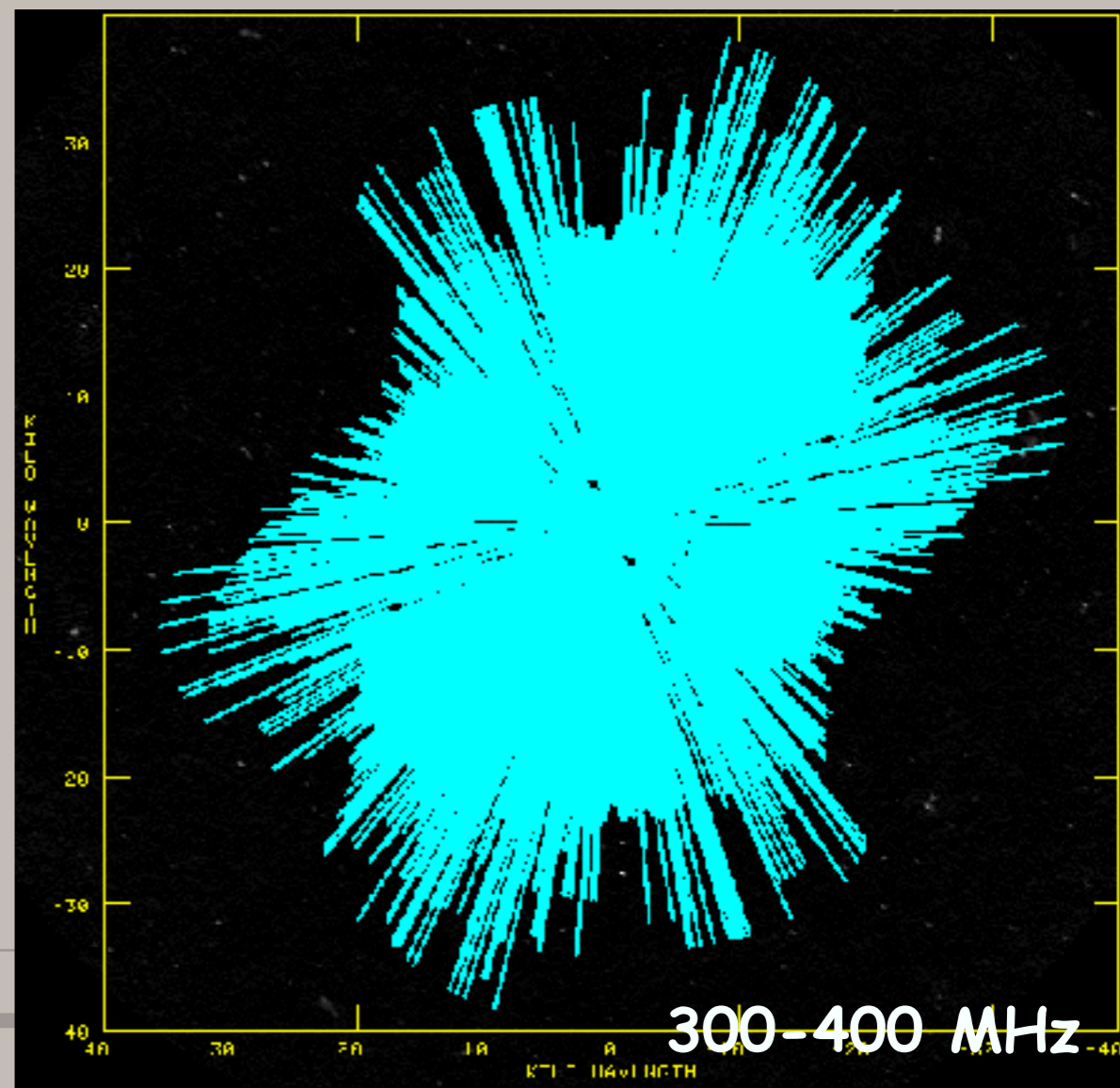
multi-frequency synthesis

$$I_{\nu}^{sky} = I_{\nu_0}^{sky} \left(\frac{\nu}{\nu_0} \right)^{I_{\alpha}^{sky} + I_{\beta}^{sky} \log(\frac{\nu}{\nu_0})}$$

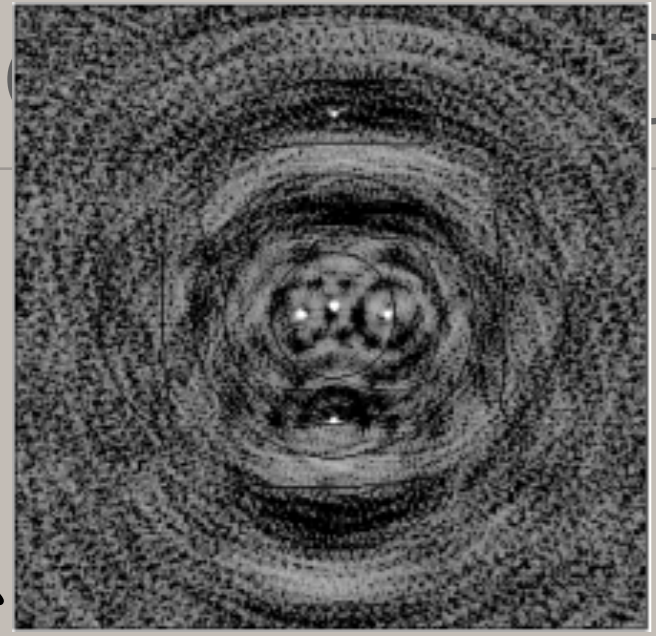
$$I_0 = I_{\nu_0}$$

$$I_1 = I_{\alpha} \times I_{\nu_0}$$

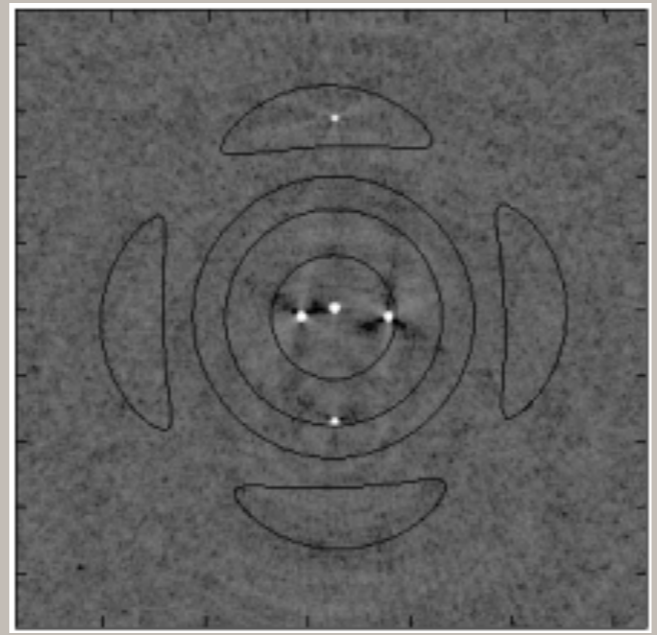
$$I_2 = (I_{\alpha}(I_{\alpha} - 1)/2 + I_{\beta}) \times I_{\nu_0}$$



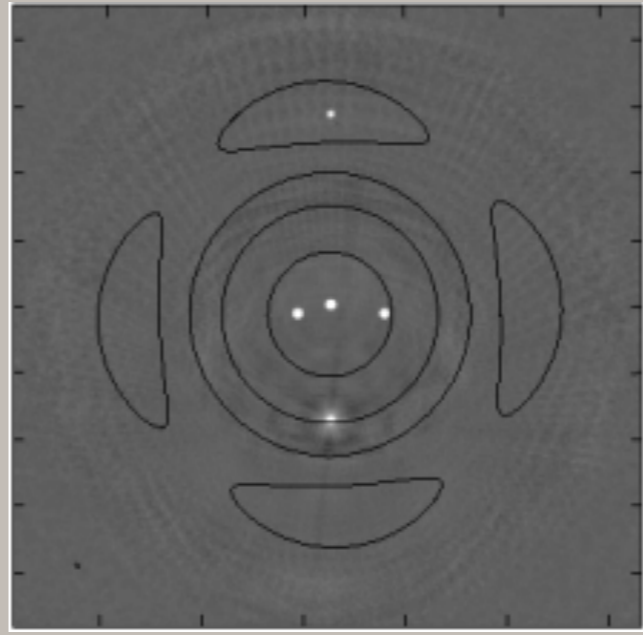
OPTION FOR **PB**



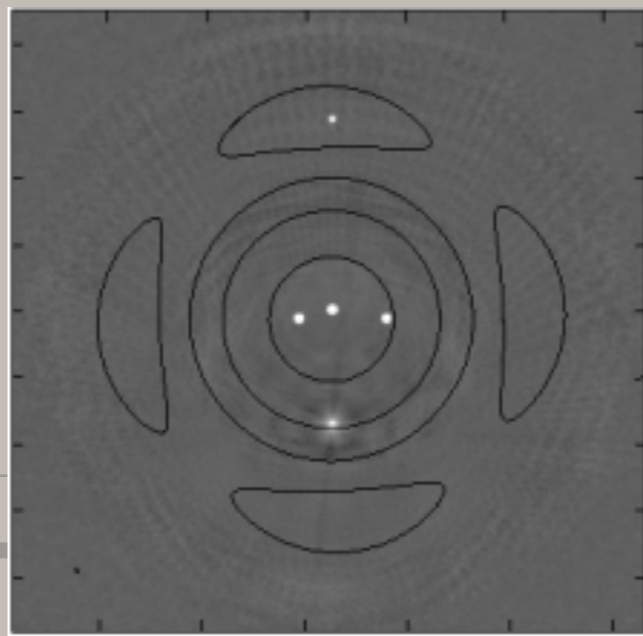
FT
(standard imaging)



FT
+ MT-MFS



FT
+ MT-MFS
+ A-projection



FT
+ MT-MFS
+ WB A-projection

Credits: S. Bhatnagar (NRAO, USA)

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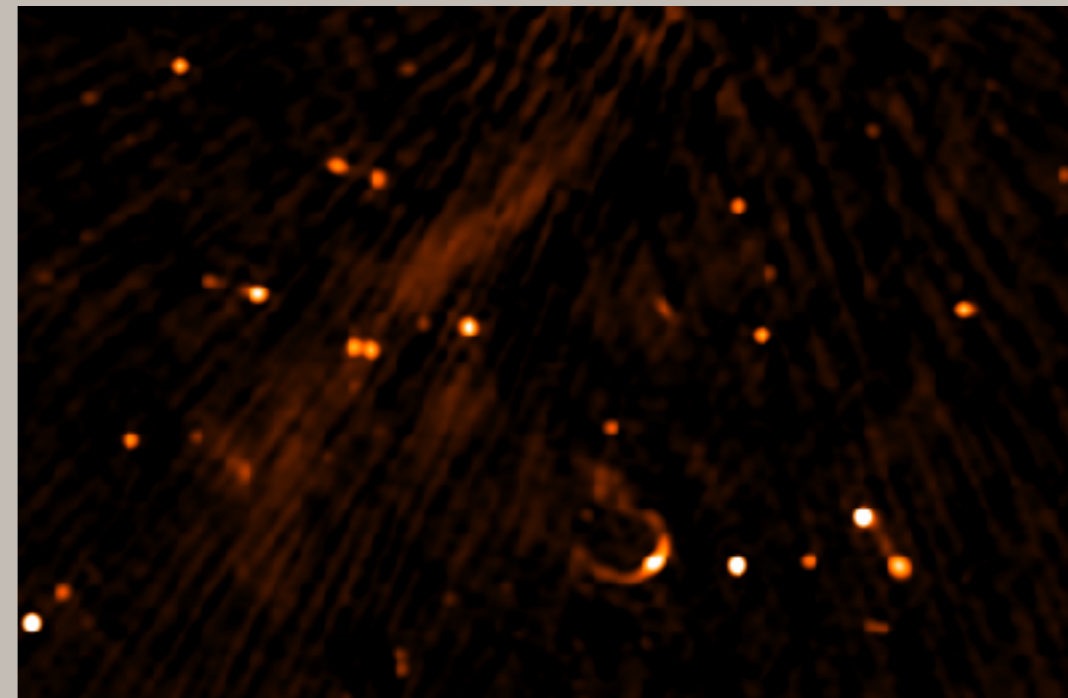
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PEELING: DD CALIBRATION

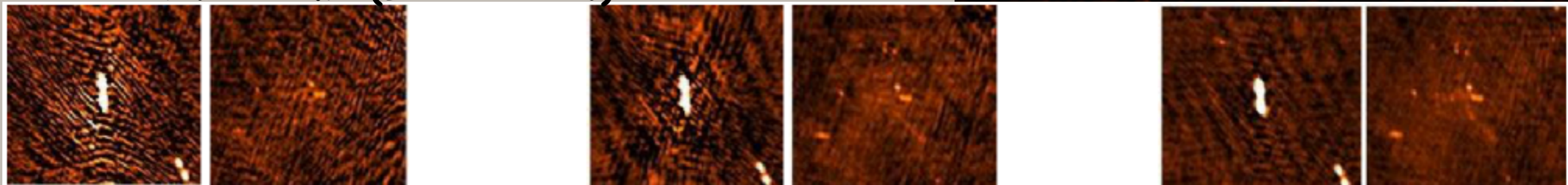
antenna based gains are determined in the direction of each compact source.

subtract these gains (contribution of compact sources from the observed data using a DFT) and the residual visibilities are imaged again.

drawbacks of peeling...



Credits: H. Intema (Leiden Obs.)



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STOKES PARAMETERS

Defined by George in 1852

- Adopted for astronomy by Chandrasehkar in 1947.
- Not a vector quantity! Deals with power instead of electric field amplitudes.
- Can be used for partially polarised radiation.
- The correlator can produce ALL Stokes parameters simultaneously (not so easy in optical astronomy!)

Stokes parameters are the auto-correlation & cross-correlation products returned from the correlator, but input to the correlator can come from different feed types.

Feeds normally designed to approximate pure linear or circular.

- Circular feeds – frequency dependent response

- adds 90° phase to R for L , so:

- I from $RR + LL$

- V from $RR - LL$

STOKES PARAMETERS

I – total intensity and sum of any two orthogonal polarisations

Q & U – completely specify linear polarisation

V – completely specifies circular polarisation

$$RR = \mathcal{A}(RR)e^{i\psi RR} = I + V$$

$$LL = \mathcal{A}(LL)e^{i\psi LL} = I - V$$

$$RL = \mathcal{A}(RL)e^{i\psi RL} = Q + iU$$

$$LR = \mathcal{A}(LR)e^{i\psi LR} = Q - iU$$

STOKES PARAMETERS

I – total intensity and sum of any two orthogonal polarisations

Q & U – completely specify linear polarisation

V – completely specifies circular polarisation

Stokes parameters (as percentages of I)

$$I = \frac{(RR + LL)}{2}$$

$$\frac{V}{I} = \frac{RR - LL}{RR + LL}$$

$$\frac{Q}{I} = \frac{\text{Re}(RL + LR)}{RR + LL}$$

$$\frac{U}{I} = \frac{\text{Im}(RL - LR)}{RR + LL}$$

STOKES PARAMETERS

I – total intensity and sum of any two orthogonal polarisations

Q & U – completely specify linear polarisation

V – completely specifies circular polarisation

Stokes parameters (as percentages of I)

Is it really that simple?

No, there are leakages...

The total intensity can leak into the polarised components (I into $\{Q, U, V\}$).

MUELLER MATRIX

The leakage of each polarisation into the other can be measured and quantified in a 4×4 matrix (Mueller 1943).

$$M = \begin{bmatrix} m_{II} & m_{IQ} & m_{IU} & m_{IV} \\ m_{QI} & m_{QQ} & m_{QU} & m_{QV} \\ m_{UI} & m_{UQ} & m_{UU} & m_{UV} \\ m_{VI} & m_{VQ} & m_{VU} & m_{VV} \end{bmatrix}$$

$$\begin{bmatrix} RR + LL \\ RL + LR \\ RL - LR \\ RR - LL \end{bmatrix} = \begin{bmatrix} m_{II} & m_{IQ} & m_{IU} & m_{IV} \\ m_{QI} & m_{QQ} & m_{QU} & m_{QV} \\ m_{UI} & m_{UQ} & m_{UU} & m_{UV} \\ m_{VI} & m_{VQ} & m_{VU} & m_{VV} \end{bmatrix} \cdot \begin{bmatrix} I \\ Q \\ U \\ V \end{bmatrix}$$

POLARISATION CALIBRATION

- Flux density scale

- $I \Leftrightarrow Q$ leakage

- $I \Leftrightarrow U$ leakage


- $I \Leftrightarrow V$ leakage

- Alignment \Rightarrow PA calibration

- Ellipticity, $Q \Leftrightarrow V$

- RL phase, $U \Leftrightarrow V$

Constrained using
calibrator with known
Stokes parameters



POLARISATION CALIBRATION

Flux density scale

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Need calibrator with
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Alignment \Rightarrow PA calibration

Ellipticity, $Q \Leftrightarrow V$

RL phase, $U \Leftrightarrow V$

Constrained using
calibrator with known
Stokes parameters

Need calibrator with
known PA

Stokes $V \sim 0$ for most
calibrators so no need to
worry too much unless you
require very high precision



PUTTING THIS ALL TOGETHER

In the end what we are trying to do is relate products from our correlator to the intrinsic polarised radiation from the source.

So we need to correct the raw correlator outputs for

- imperfections in the receiver (leakages).

- The orientation of the receiver with respect to the telescope structure.

- a.k.a. the changing parallactic angle.

- Any measured propagation related polarisation effects (e.g. Faraday rotation).

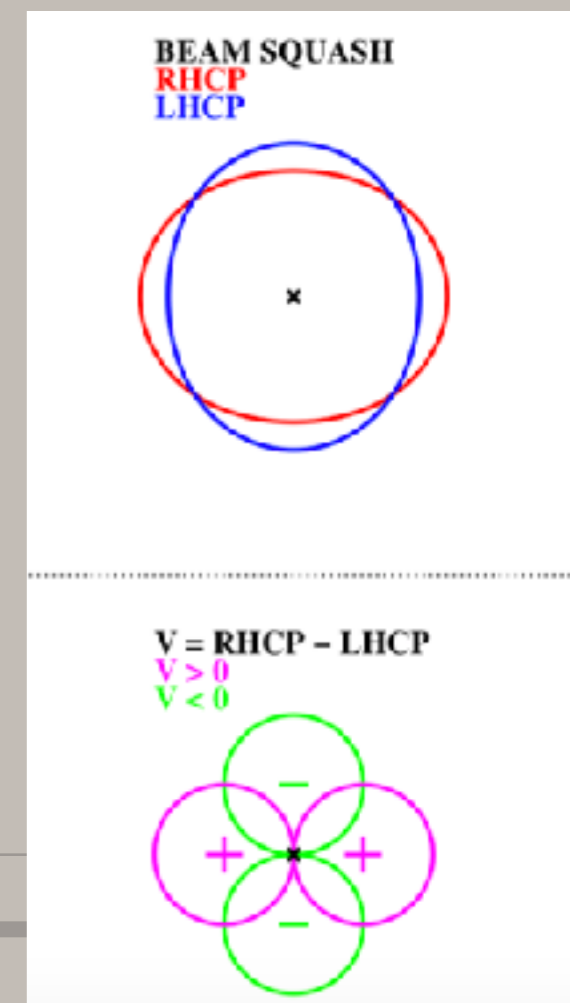
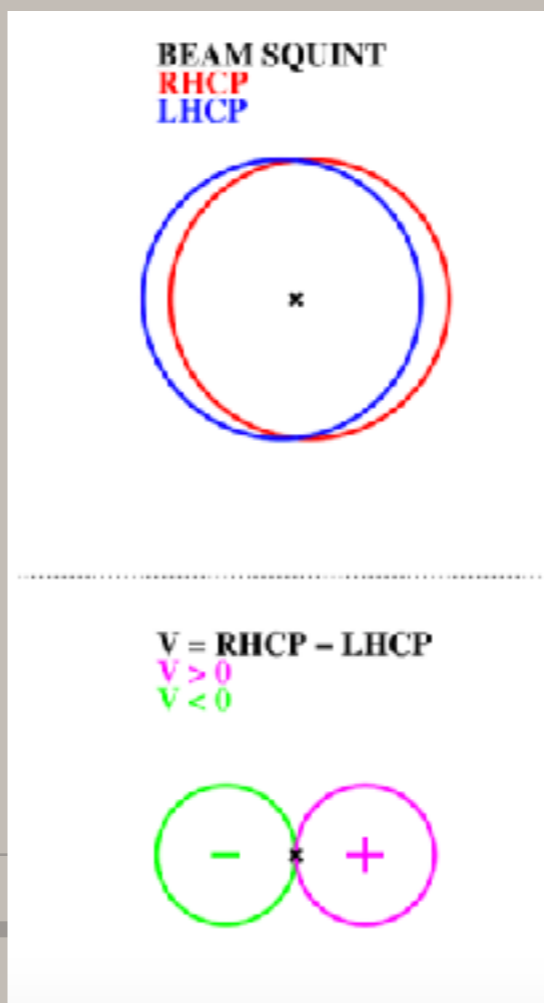
BEAM EFFECTS

For point sources, all of the previous is fine.

What if the source you are looking at is extended compared to the telescope beam?

There are instrumental beam effects that can confuse the measurement of extended polarised signals. They are...

- Squint
- Squash



BEAM EFFECTS

$$\vec{V}_{ij}^{Obs}(\nu, t) = W_{ij}(\nu, t) \int M_{ij}(s, \nu, t) \vec{I}(s, \nu) e^{i\vec{b}_{ij} \cdot \vec{s}} d\vec{s}$$



DATA



Weights



Mueller
matrix



full-polarization
vector of the sky
brightness
distribution

BEAM EFFECTS

$$\vec{V}_{ij}^{Obs}(\nu, t) = W_{ij}(\nu, t) \int M_{ij}(s, \nu, t) \vec{I}(s, \nu) e^{i\vec{b}_{ij} \cdot \vec{s}} d\vec{s}$$

$$M_{ij}(\vec{s}, \nu, t) = E_i(\vec{s}, \nu, t) \otimes E_j^*(\vec{s}, \nu, t)$$

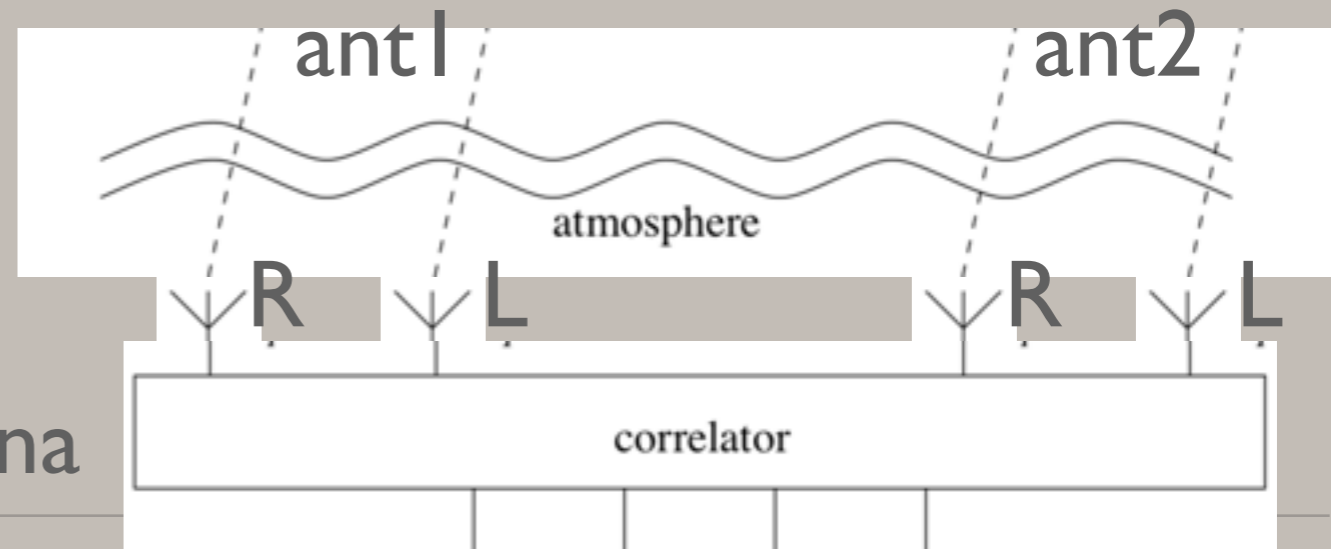
$$\vec{V}_{ij}^{Obs}(\nu, t) = W_{ij}(\nu, t) \mathcal{F} \left[\left(E_i(\vec{s}, \nu, t) \otimes E_j^*(\vec{s}, \nu, t) \right) \cdot \vec{I}(\vec{s}, \nu) \right]$$

$$= W_{ij}(\nu, t) \left[A_{ij} \star \vec{V}_{ij} \right]$$

$$\text{where, } A_{ij} = A_i \otimes A_j^*$$



AIPs for two antenna



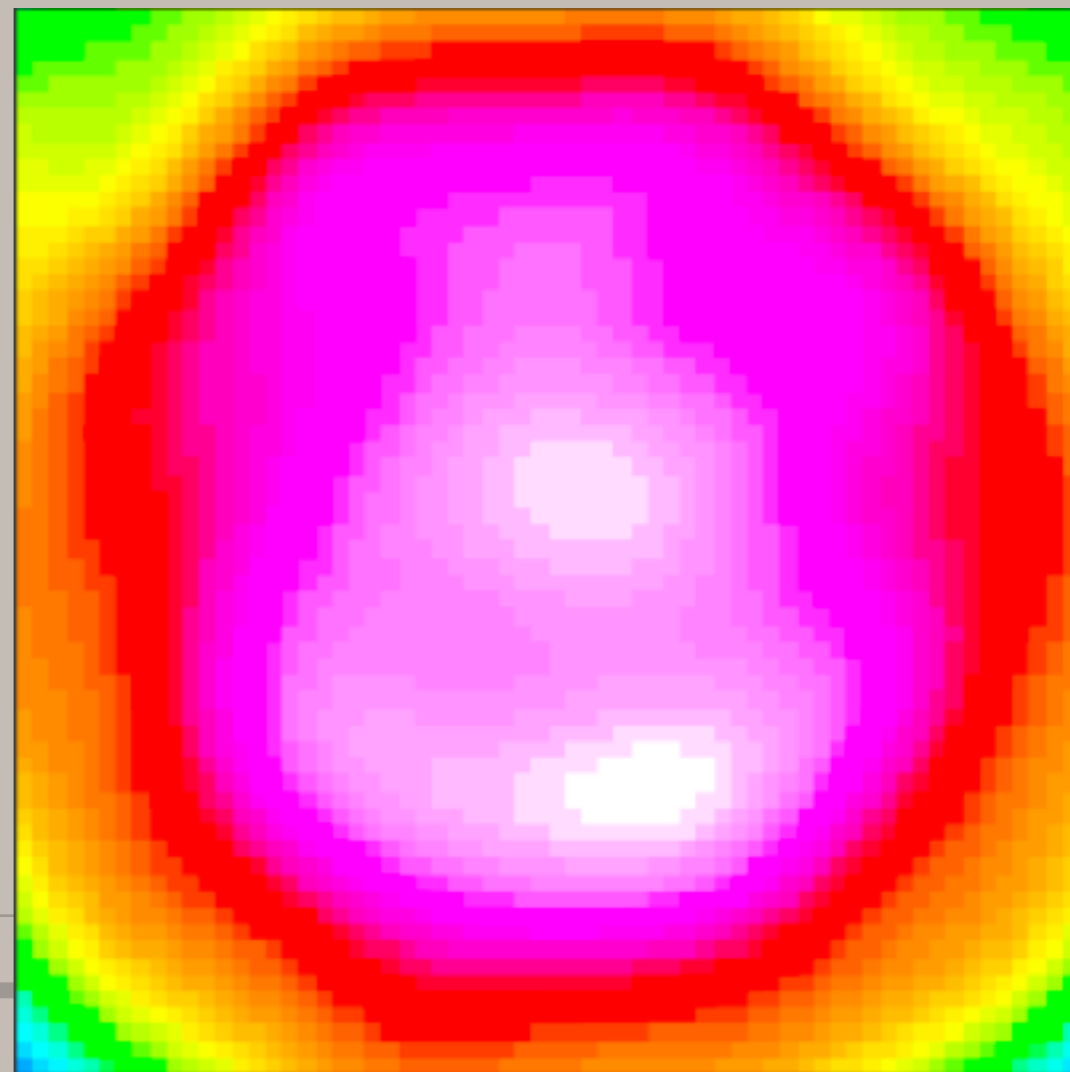
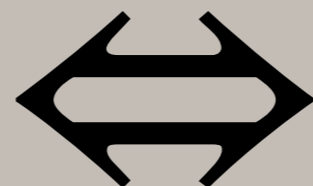
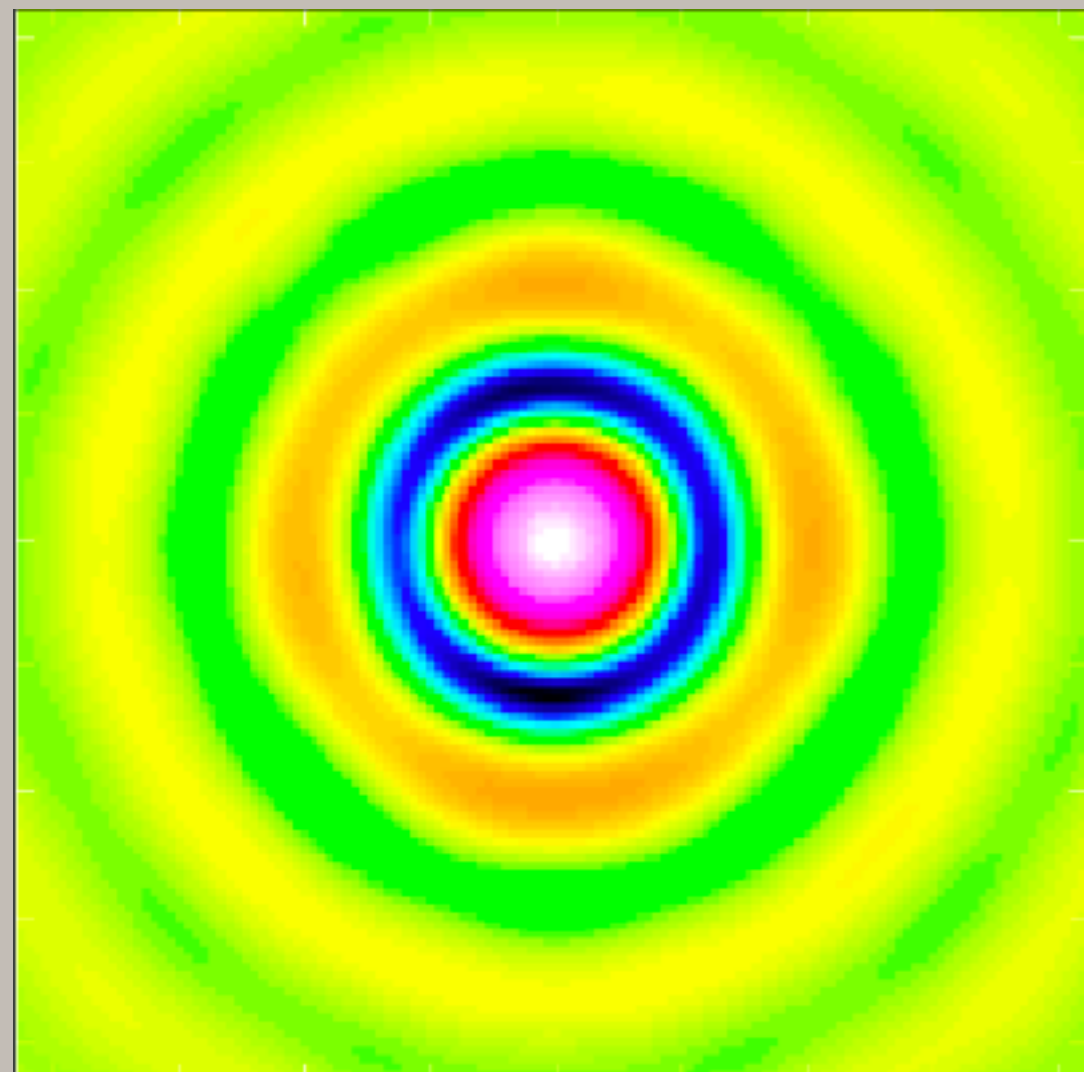
APERTURE ILLUMINATION PATTERN

Holography data: MeerKAT

Obtained by Fourier Transforming
the PB Holography measurements



Credits: S. Sekhar (UCT-IDIA)

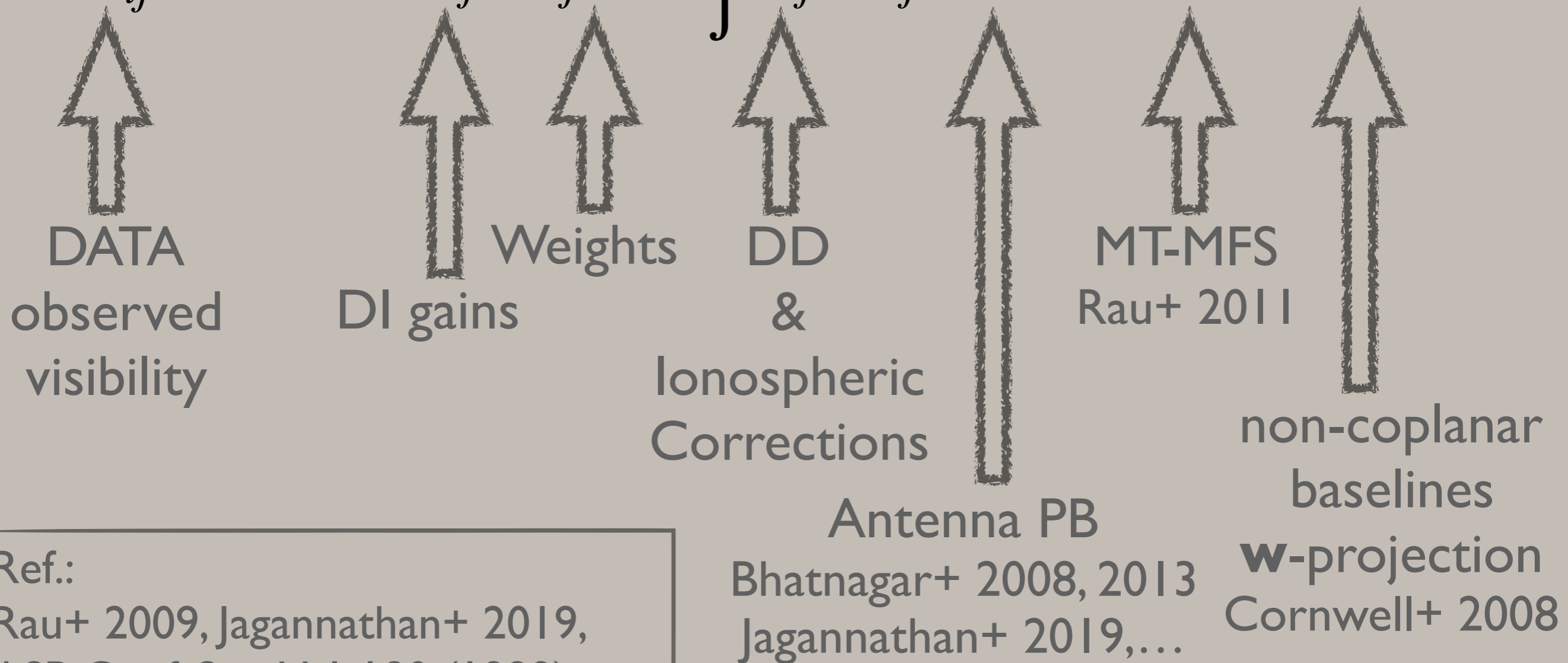


A-TO-Z SOLVER

- Use Zernike polynomials to directly model the complex aperture
 - it is a natural domain to model optical aberrations that cause PB weirdness
 - (Telescope agnostic - does not require ray traced model for different antennas/telescopes, only Holography)
 - Aperture size is fixed, independent of number of measured sidelobes.

MEASUREMENT EQUATION

$$\vec{V}_{ij}^{Obs}(\nu, t) = G_{ij} W_{ij}(\nu, t) \int P_{ij} M_{ij}(s, \nu, t) \vec{I}(s, \nu) e^{i\vec{b}_{ij} \cdot \vec{s}} d\vec{s}$$



Ref.:
Rau+ 2009, Jagannathan+ 2019,
ASP Conf. Ser. Vol. 180 (1999)

Bhatnagar+ 2008, 2013
Jagannathan+ 2019,...

w-projection
Cornwell+ 2008

Thank you all for your attention!