# INTERFEROMETRY





(Courtesy: ASTRON, NRAO, ATNF, SARAO, GMRT)

(Rick Perley, Frank Schinzel)

## WHY INTERFEROMETRY?

• Angular resolution ~  $\lambda/D \Rightarrow$  Need a *huge* single dish for high resolution.





(Courtesy: NRAO, Jeff Dai)

• Angular resolution of ~ 1''  $\Rightarrow$  Dish diameter ~ 42 km!!!

### INTERFEROMETRY: PHILOSOPHY

• Single dish: Coherent sum of electromagnetic fields at the dish focus.

- Interferometer: Combine voltages of many small dishes, keeping phase information.
- Dishes do not need to be next to each other.



### INTERFEROMETRY: PHILOSOPHY



<sup>(</sup>Courtesy xkcd.com/1922)

### SIGNALS AND DETECTORS

- Distant radiation source of intensity I(v,s).
- Detector of area A(v,s).
- Power dP from a small solid angle  $d\Omega$ and a small frequency interval dv:  $dP = A(v,s).I(v,s).dv.d\Omega$ .
- Total power,  $P = \iint A(v,s).I(v,s).dv.d\Omega$ .



(Rick Perley, NRAO lectures)

#### QUASI-MONOCHROMATIC INTERFEROMETER

• Distant source of quasi-monochromatic radiation:  $E_v(t) = E.Cos[2\pi vt]$ .



• "Cosine correlator": Output depends on the baseline length, orientation. Does *not* depend on time, source distance, baseline location.

### The Fringe Pattern

θ

α

b.s/λ = u.Cosα = u.l
u ≡ Baseline length in wavelengths.
1 ≡ Direction cosine.
⇒ R<sub>C</sub> = P.Cos(2π u.l)



• Fringe angular spacing,  $\Delta \theta \sim (\lambda/b)$ .

(Courtesy: Rick Perley)

### The Fringe Pattern

Long baselines ⇒ Finer fringes.
 Short baselines ⇒ Wider fringes.



(Courtesy: Rick Perley)

### The Interferometer Response

- For an extended source  $\Rightarrow R_C = \int A(s) \cdot I(s) \cdot Cos(2\pi \mathbf{b} \cdot \mathbf{s}/\lambda) d\Omega$
- Throws a sinusoidal fringe pattern on the sky, multiples the sky intensity by the fringe pattern, and then integrates over the sky.

### THE INTERFEROMETER RESPONSE

#### • CygnusA with a 5-km baseline at $\sim 2$ GHz.





(Courtesy: Rick Perley)

### The Interferometer Response

- For a "point source", same interferometer response for all baselines.
- The interferometer response can be negative for a real source!
- The interferometer response tends to zero for the longer baselines: Sources get "resolved out".
- The interferometer response tends to the total flux density for shorter baselines: The "zero spacing flux".
- $R_C = \int A(s) \cdot I(s) \cdot Cos(2\pi b.s/\lambda) d\Omega$ Sensitive to the "even" part of the sky intensity distribution.
- Not sufficient to recover the "true" sky intensity distribution!
   ⇒ Need an "odd" fringe function.

#### THE SINE CORRELATOR

• 90-degree phase shift in one of the signal paths!



• For an extended source  $\Rightarrow R_S = \int A(s) \cdot I(s) \cdot Sin(2\pi \mathbf{b} \cdot \mathbf{s}/\lambda) d\Omega$ 

#### THE COMPLEX CORRELATOR

- Define the complex visibility  $V = R_C i.R_S = A \cdot e^{-i\phi}$ where  $A = [R_C^2 + R_S^2]^{\frac{1}{2}}$  and  $\phi = Tan^1 [R_C/R_S]$
- $R_C = \int A(s) \cdot I(s) \cdot Cos(2\pi b.s/\lambda) d\Omega$  $R_S = \int A(s) \cdot I(s) \cdot Sin(2\pi b.s/\lambda) d\Omega$

$$\Rightarrow$$
 Visibility V<sub>v</sub>(**b**) = R<sub>C</sub> - i.R<sub>S</sub> =  $\int A(\mathbf{s}) \cdot I(\mathbf{s}) \cdot e^{-2\pi i \mathbf{b} \cdot \mathbf{s}/\lambda} d\Omega$ 

• General relation between complex visibility and sky intensity!

#### COORDINATE SYSTEMS

- The baseline **b** has components  $\lambda(u,v,w)$ .
- For the unit vector **s**, the co-ordinates in the (u, v, w) system are the direction cosines  $1 = \cos(\alpha)$ ,  $m = \cos(\beta)$ , and  $n = \cos(\gamma)$ .  $l^2 + m^2 + n^2 = 1$



•  $\mathbf{b} \cdot \mathbf{s}/\lambda = (\mathbf{u}\mathbf{l} + \mathbf{v}\mathbf{m} + \mathbf{w}\mathbf{n}) = \mathbf{u}\mathbf{l} + \mathbf{v}\mathbf{m} + \mathbf{w}\{(1 - 1^2 - m^2)^{1/2} - 1\}$  $d\Omega = d\mathbf{l} \cdot d\mathbf{m}/\mathbf{n} = (1 - 1^2 - m^2)^{-1/2} d\mathbf{l} \cdot d\mathbf{m}$ 

•  $V_v(u,v,w) = \iint A_v(l,m) I_v(l,m) \cdot e^{-2\pi i [ul+vm+w\{(1-l^2-m^2)^{1/2}-1\}]} \cdot (1-l^2-m^2)^{-1/2} dl.dm$ 

• Note: This is *not* a Fourier transform relation!!!

#### SPECIAL CASES

• All visibility measurements in a single plane, i.e.  $w \approx 0$ .

• $\Rightarrow$  V<sub>v</sub>(u,v,w) =  $\iint A_v(1,m) \cdot I_v(1,m) \cdot e^{-2\pi i \cdot [ul+vm]} \cdot (1 - l^2 - m^2)^{-1/2} dl.dm$ 

 $\Rightarrow$  2-D Fourier transform between V<sub>v</sub>(u,v) and I<sub>v</sub>(l,m) × (1 - l<sup>2</sup> - m<sup>2</sup>)<sup>-1/2</sup> !

• All sources in a small sky region: i.e. w.n  $\approx 0$  for non-zero I<sub>v</sub>(1,m).

• 
$$\Rightarrow$$
 V<sub>v</sub>(u,v) =  $\iint A_v(1,m) \cdot I_v(1,m) \cdot e^{-2\pi i [ul+vm]} dl.dm$ 

- $\Rightarrow$  2-D Fourier transform between  $V_v(u,v)$  and  $A_v(l,m)$ .  $I_v(l,m)!$
- At low frequencies, cannot assume all sources in a small sky region. Must correct for 3-D effects: Faceting or w-projection. (Cornwell et al. 2008, IEEE)
- One measures  $V_v(u,v)$  and then obtains the sky intensity  $I_v(l,m)$  by A(l,m). $I_v(l,m) = \iint V_v(u,v) \cdot e^{2\pi i [ul+vm]} du.dv$

### RADIO INTERFEROMETRY

• The visibility  $V_v(u,v)$  is related to the sky intensity distribution  $I_v(l,m)$ :  $V_v(u,v) \approx \iint A_v(l,m) \cdot I_v(l,m) e^{-2\pi i(ul + vm)} dl dm$ 

(u,v,w) are components of the baseline; (l,m) are direction cosines.

- Measure *cross-correlations* of the voltages determined at different antennas, as a function of each antenna antenna baseline. Then carry out a 2-D Fourier transform to infer the sky intensity distribution.
- As the Earth rotates, the separation of a pair of antennas relative to the source direction will change! Each antenna pair measures V(u,v) at a *changing* (u,v) location with time, yielding a curve in the u-v plane, and hence, better sampling of this plane!

⇒ Earth-rotation Aperture Synthesis

➡ Distribute your antennas so as to obtain the best (most uniform) coverage of the 2-D u-v plane, for *all* directions.

### ARRAY CONFIGURATIONS

• Y-shaped array optimal for  $\sim 20 - 40$  antennas (VLA, GMRT). Random or spiral array for more than  $\sim 50$  antennas (ALMA, LOFAR).

(Courtesy: NRAO)





 VLA: 27 antennas on rails in a Y-array. Moved every 4 months to get different u-v coverage. Longest baseline ~ 1 km, 3.3 km, 11 km, 35 km.

• GMRT: 30 fixed antennas, 14 in a 1-km central square, 16 in Y-array.

### ARRAY U-V COVERAGE: THE VLA

• The set of all baseline vectors during the observations. Its 2-D Fourier transform is the synthesized beam. Observing a source for even a few hours gives a much better u-v coverage and a "cleaner" beam.



### ARRAY U-V COVERAGE: THE GMRT



• Dense patches due to the large number of central square antennas.

### ARRAY U-V COVERAGE: THE GMRT

(Patra et al. 2018, MNRAS)



• "Reasonable" u-v coverage at all declinations in a 12-hr track.

### RESOLUTION

• Radio interferometry: Far better angular resolution than in the optical!



 $\lambda \sim 6000$ Å, D = 2.4m  $\Rightarrow$  R ~ 0.05 arcsec



 $\lambda \sim 7mm$ , D  $\sim 35 \text{ km}$  $\Rightarrow R \sim 0.04 \text{ arcsec}$ 



 $\lambda \sim 0.3$ mm, D ~ 16 km  $\Rightarrow$  R ~ 4 milli-arcsec



 $\lambda \sim 7mm$ , D ~ 10,000 km  $\Rightarrow R \sim 0.15$  milli-arcsec

(Courtesy: NRAO, NASA)